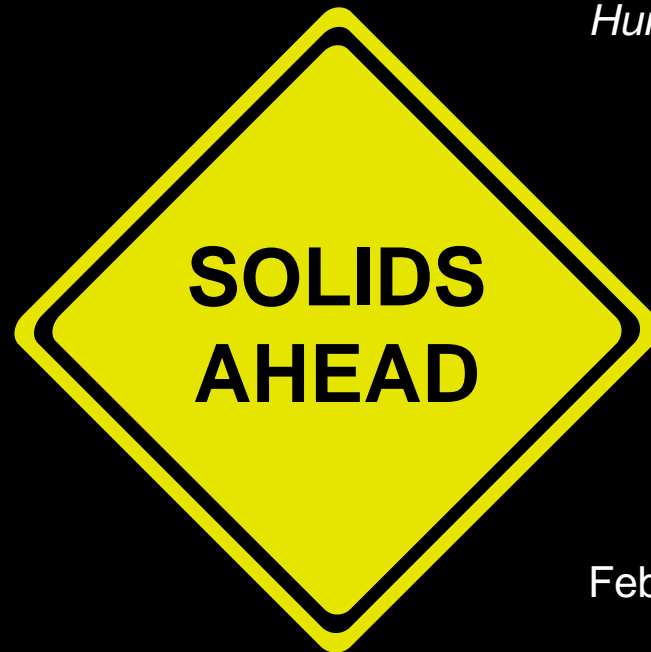


Evaluating Self Cleansing in Existing Sewers Using the Tractive Force Method

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Background

Gravity Sanitary Sewer Design and Construction, 2nd Ed. 2007

Joint publication: ASCE Manual No.60 / WEF MOP FD-5

Previous Editions:

1982

1962

1935

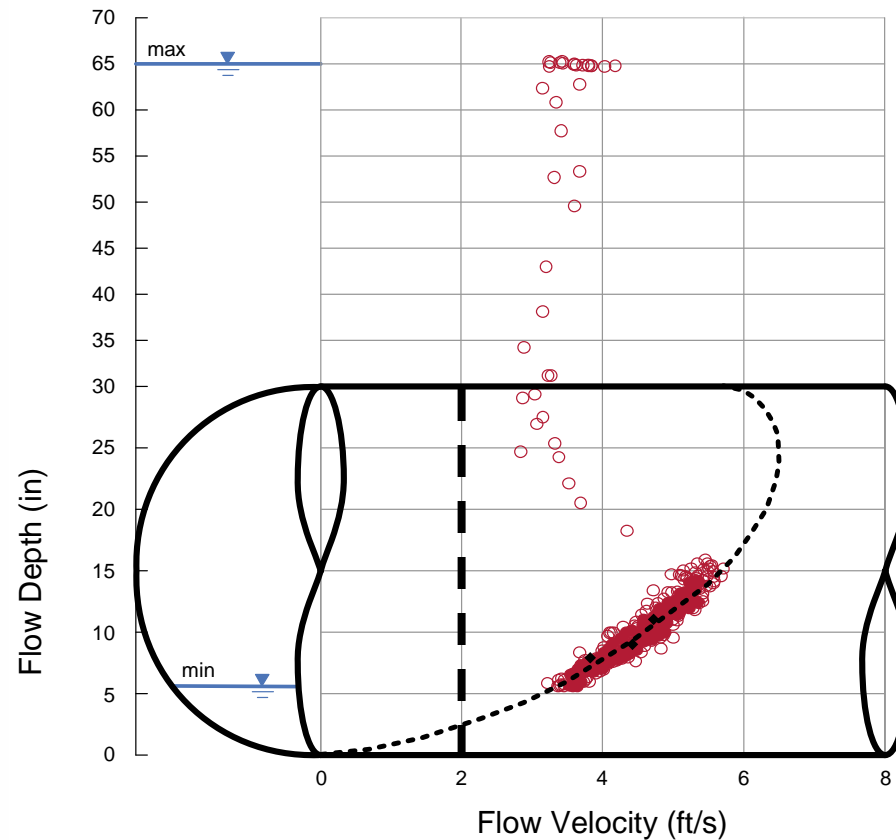
Self Cleansing Information History

2007 – 18 pages

1982 – 1.5 pages

What is a Scattergraph?

$$v = \frac{1.486}{n} R^{2/3} S^{1/2}$$



Enfinger, K.L. and Keefe, P.N. (2004). "Scattergraph Principles and Practice – Building a Better View of Flow Monitor Data," KY-TN Water Environment Association Water Professionals Conference; Nashville, TN.

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Shear Stress

Self-cleansing conditions within a sewer are directly related to **shear stress**. As wastewater flows within a sewer, it exerts an average shear stress, or tractive force, on the sewer as shown below.

$$\tau = \gamma RS$$

where:

- τ = average shear stress, lb/ft²
- γ = specific weight of water, lb/ft³
- R = hydraulic radius, ft
- S = slope of the energy gradient, ft/ft

Flow conditions are classified as self-cleansing when the actual shear stress (τ) is greater than or equal to a specified critical shear stress (τ_c) at a defined frequency of occurrence.

Wastewater Solids Characteristics in the United Kingdom

Solids Type	Transport Mode	Median Size d_{50}			Specific Gravity		
		mm					
		Low	High	Low	High
Sanitary	Suspension	0.01	0.04	0.06	1.01	1.40	1.60
Storm Water	Suspension	0.02	0.06	0.10	1.10	2.00	2.50
Grit	Bedload	0.30	0.75	1.00	2.30	2.60	2.70

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design particle = 1.0-mm grit particle with specific gravity of 2.70

Critical Shear Stress

Raths and McCauley have previously investigated the **critical shear stress** needed to transport grit particles of various sizes as bedload within a sewer. Their results are presented in equation form as shown below.

$$\tau_c = 0.0181(D_p)^{0.277}$$

where: τ_c = critical shear stress, lb/ft²
 D_p = particle size, mm

Based on the selected design particle, a critical shear stress of 0.0181 lb/ft² is needed to achieve self-cleansing conditions.

Critical Shear Stress Translated to Flow Velocity

$$\tau = \gamma RS \quad \rightarrow \quad S = \frac{\tau_c}{\gamma R}$$

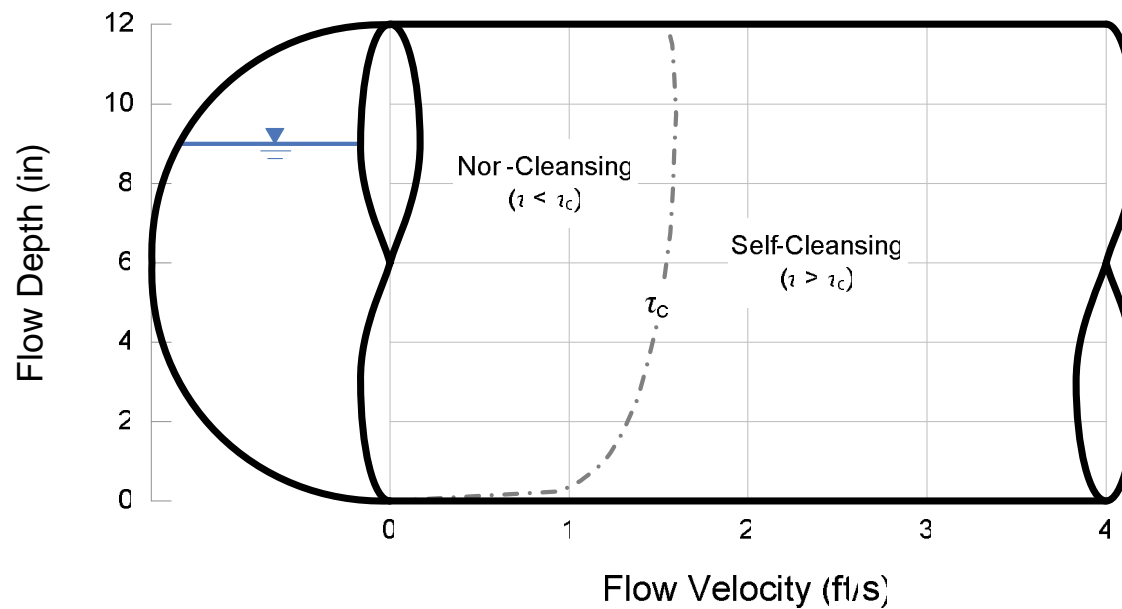
$$v = \frac{1.486}{n} R^{2/3} S^{1/2} \quad \rightarrow \quad v_{sc} = \frac{1.486}{n} R^{1/6} \left(\frac{\tau_c}{\gamma} \right)^{1/2}$$

where:

- v_{sc} = self-cleansing flow velocity, ft/s
- n = roughness coefficient
- R = hydraulic radius, ft
- τ_c = average shear stress, lb/ft²
- γ = specific weight of water, lb/ft³

Critical Shear Stress Displayed Graphically

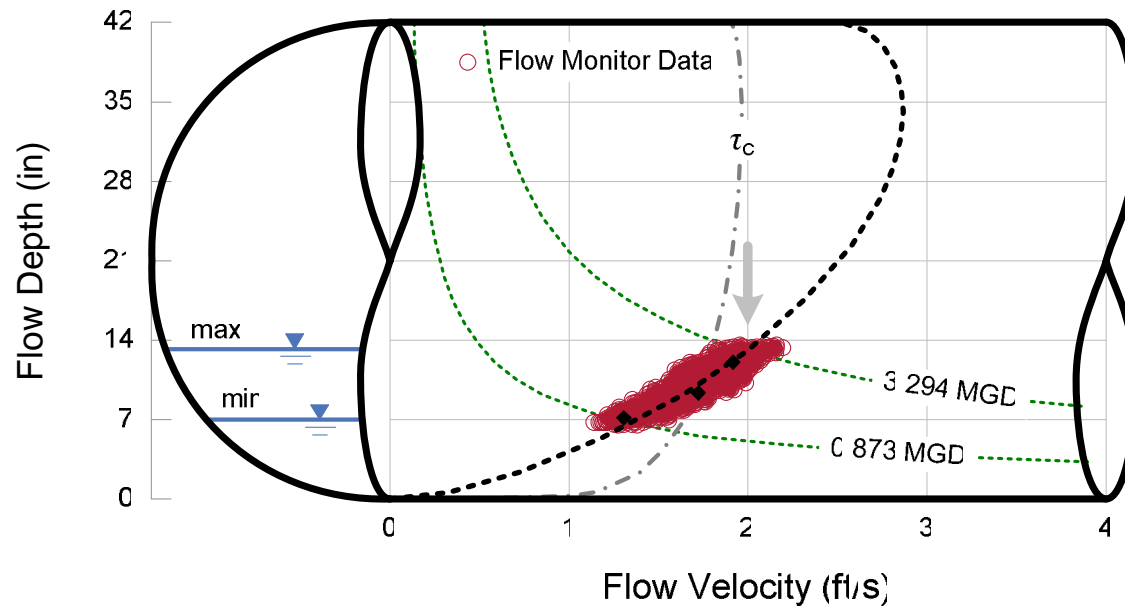
$$v_{sc} = \frac{1.486}{n} R^{1/6} \left(\frac{\tau_c}{\gamma} \right)^{1/2}$$



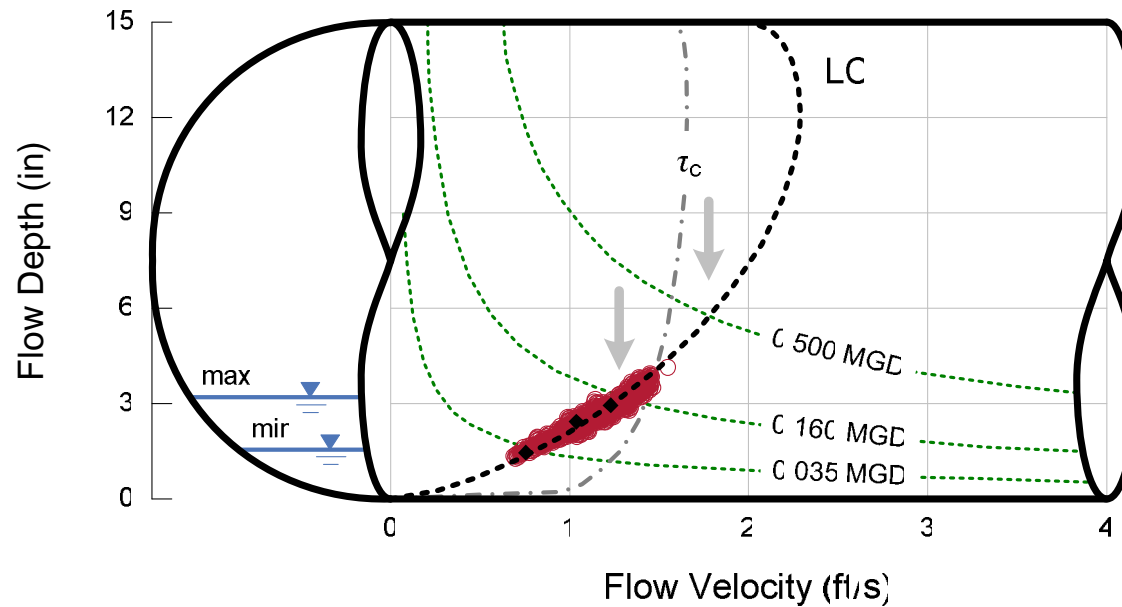
Moraitis, P. (1999). "Development of Gravity Flow Pipe Design Charts." Unpublished Undergraduate Project for Professor David Butler. Imperial College, Department of Civil and Environmental Engineering, London.

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Self-Cleansing Conditions

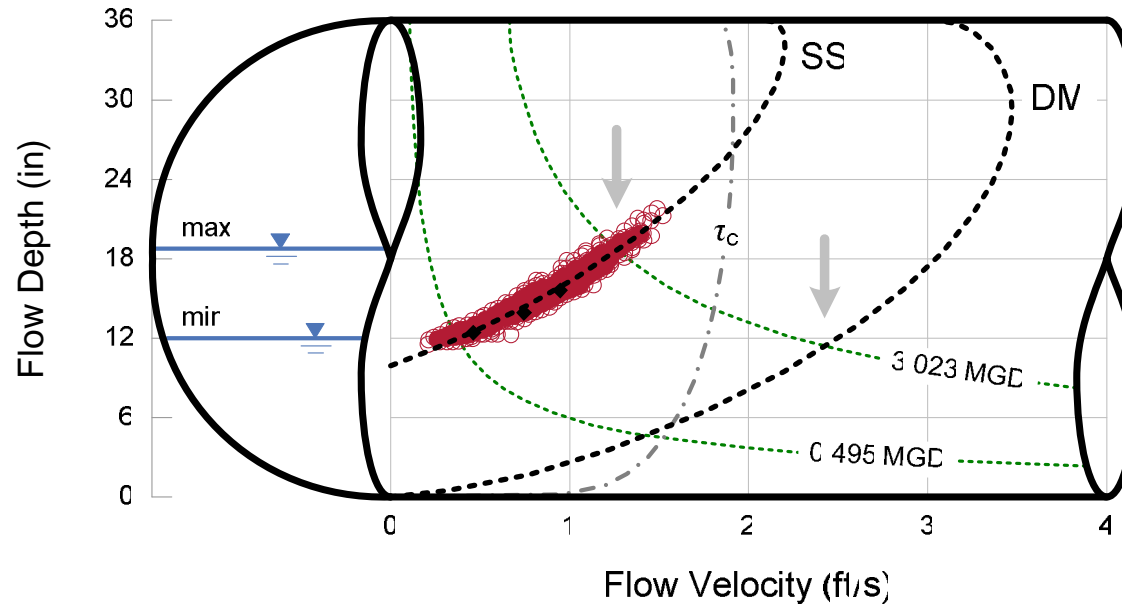


Non-Cleansing Conditions – Type I



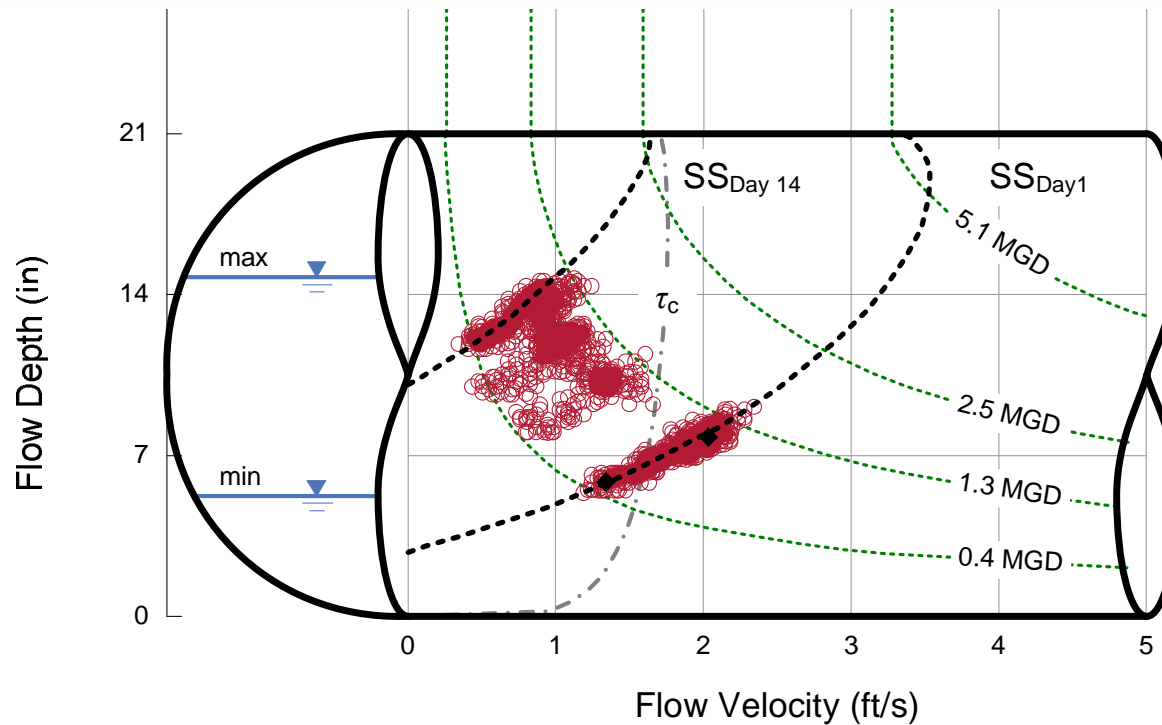
Type I non-cleansing conditions include sewers that operate under uniform flow conditions, but do not have conditions necessary to generate a shear stress in excess of the required critical shear stress.

Non-Cleansing Conditions – Type II



Type II non-cleansing conditions include sewers that operate under non-uniform flow conditions caused by backwater effects resulting from a variety of downstream obstructions, or *dead dogs*. Examples include offset joints, debris, and other related conditions.

Non-Cleansing Conditions – Type II



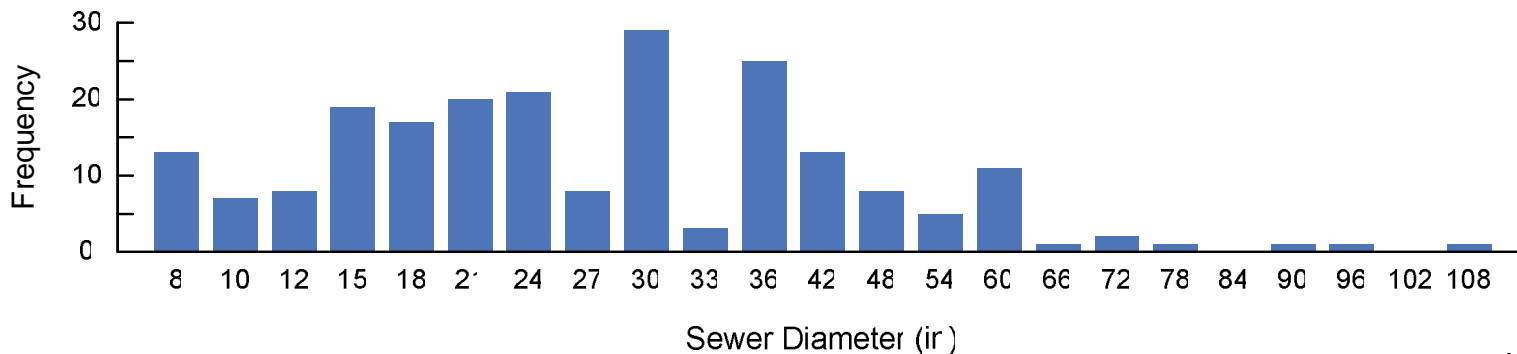
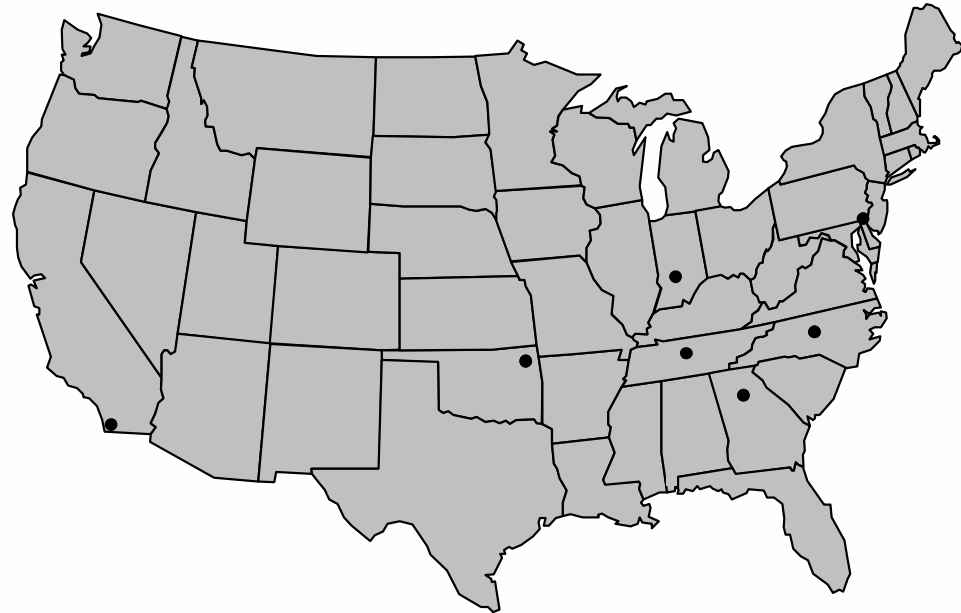
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A Practical Test of the Tractive Force Method

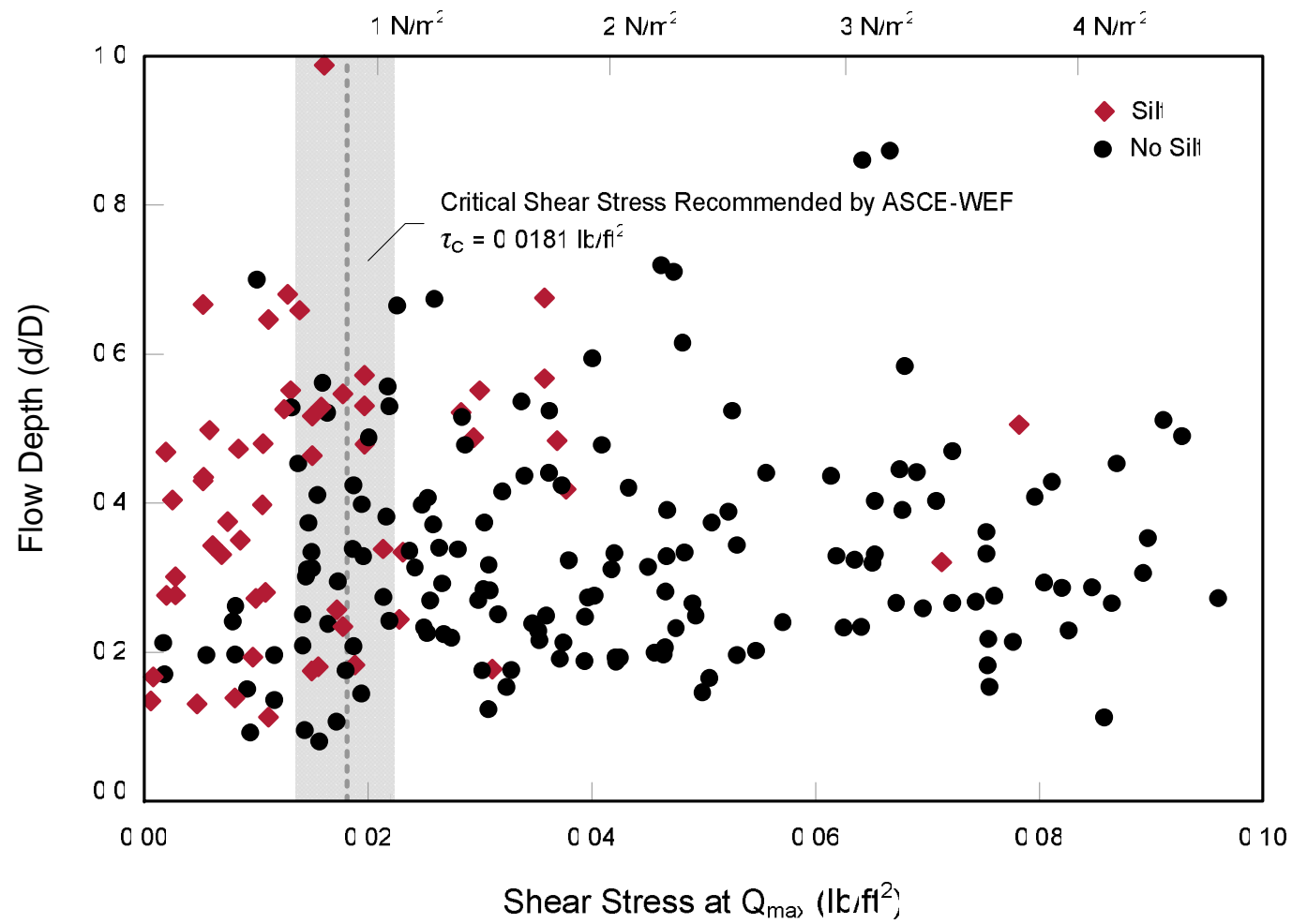
Flow monitor data were obtained from 214 existing sewers during a 30-day evaluation period.

Each sewer was classified as self-cleansing or non-cleansing, based on the **Tractive Force Method**.

Independent silt measurements were then obtained over a 12-month Observation Period and compared to original predictions.



Test Case Summary



Conclusion

- ❖ Previous self cleansing design criteria result in slopes that are steeper than needed for smaller pipes (<42”) and flatter than actually needed for larger pipes.
- ❖ Existing sewers with adequate self-cleansing conditions and those with potential silt, sediment, or debris accumulation are readily identified looking at flow data scattergraphs.
- ❖ Practical application of this method to over 200 existing sewers demonstrates the general effectiveness of the tractive force approach for the self-cleansing design of sanitary sewers.

Questions or Comments?

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